

MAP 1. SLOPE OF LAND SURFACE

Quadrangle Atlas No.20

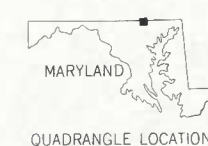


EXPLANATION

This map shows the slope of the land surface in the New Freedom quadrangle, with the slope values grouped into categories. The map was prepared from a 1:24,000-scale topographic contour plate using a semi-automatic photomechanical process. In this process, a device measures the distance between adjacent lines and, for the contour interval provided, calculates the slope between the lines. Narrow summits or depressions and similar features may be falsely mapped due to the bending of a line upon itself. Likewise, equal but adjacent contours produce over-estimated slopes. Widely separated contour lines may result in an averaging of the intervening slopes. These limitations are only of small extent. The slope categories, which relate to those in the Baltimore County Soil Survey, were selected for their relevance to current and contemplated Baltimore County planning regulations.

SCALE 1:24,000
1 000 2000 3000 4000 5000 6000 7000 FEET
1 KILOMETRE
CONTOUR INTERVAL 20 FEET
NATIONAL GEODETIC VERTICAL DATUM OF 1929

1983

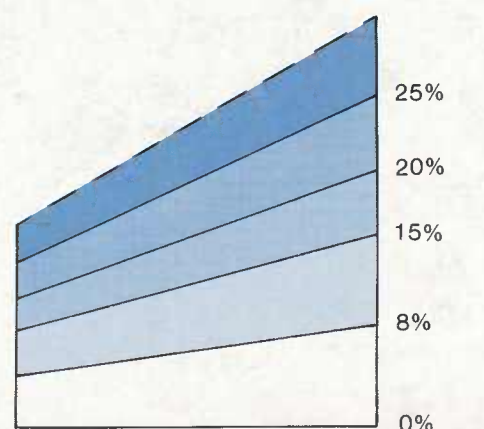


QUADRANGLE LOCATION



UTM GRID AND 1971 MAGNETIC NORTH
DECLINATION AT CENTER OF SHEET

Prepared by Photo Science, Inc., Gaithersburg
Maryland. Utilizing contour negatives, furnished
by United States Geological Survey.



MAP 2. LOCATIONS OF WELLS AND SPRINGS

EXPLANATION																
Information for some of the wells on this map (comprising an earlier inventory) is tabulated in the Maryland Geological Survey Basic Data Report No. 1 (Laughlin, 1966). Supplementary wells are tabulated in this atlas. The supplementary well information has been entered in the National Water Data Storage and Retrieval System (NWDS) of the U. S. Geological Survey and is available from the office of the USGS in Towson, Md.																
Since 1945, the State of Maryland has required a permit to drill a water well. The numbers corresponding to the permit applications are included in the well-data tabulations. Since 1973, these numbers have appeared on metal tags affixed to the well casings. Much of the well data collected for this report is obtained from well-completion forms which the well driller must submit to the State upon completion of the well. Well drillers obtain discharge data by various methods, such as filling a bucket, using a flowmeter, or estimation.																
LOCAL NUMBER	STATE NUMBER	OWNER	CONTRACTOR	DATE COMPLETED	ALTITUDE OF LAND SURFACE (FEET)	DEPTH OF WELL (FEET)	FINISH (FEET)	CASING DEPTH (FEET)	PRINCIPAL AQUIFER	WATER LEVEL (FEET)	DISCHARGE (GALLONS PER MINUTE)	DATE MEASURED	PUMPING PERIOD (HOURS)	SPECIFIC CAPACITY (GPM/FT)	USE OF WATER	FINISH CODE
BA AC 88	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 89	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 90	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 91	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 92	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 93	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 94	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 95	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 96	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 97	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 98	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 99	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 100	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 101	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 102	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 103	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 104	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 105	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 106	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 107	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 108	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 109	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 110	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 111	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 112	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 113	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 114	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 115	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 116	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 117	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 118	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 119	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 120	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 121	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 122	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 123	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 124	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 125	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 126	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 127	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 128	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 129	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 130	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 131	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 132	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 133	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 134	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 135	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 136	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 137	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 138	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 139	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 140	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 141	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 142	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 143	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 144	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 145	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 146	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 147	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 148	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/1976	200.0	10	190.0	23	A	300PMH	19.0	06/19/1976	4.0	0.1	H	5
BA AC 149	HA-73-1097	MILTON, HUGHES H	W. W. WICKHAM	06/19/19												

MAP 3. DEPTH TO WATER TABLE

DEPTH TO THE WATER TABLE

By
Mark T. Duigon

EXPLANATION

This map shows the distance from the land surface to the water table (top of the zone of saturation). The map is based on well-drillers' completion reports supplemented by soils maps and observations of springs, swamps, and other natural features. The map shows that the water table is generally shallowest near streams, and deepest under summits of hills and ridges.

The position of the water table is not constant, but responds to various stresses, chiefly precipitation and evapotranspiration. The water table is usually highest during the early spring and lowest in late summer and early fall. Precipitation tends to raise the water table, but much of this water may be removed by evapotranspiration before reaching the zone of saturation. This removal of water is most notable during the growing season. Springflow may fluctuate with changes in the position of the water table. A spring that usually flows all year may cease to discharge during a prolonged drought, because the water table has declined to a point below the land surface. The map presented here is generalized, showing average depths to the water table.

Figure 1 shows a 19-year record of water levels in well BA-CE 21 measured periodically by the U.S. Geological Survey. This well, located near Jacksonville, Md., shows the seasonal variations that are characteristic of most water-table wells. It also shows variations in annual mean levels.

A discharging well produces a lowering of the water table (drawdown), but, in the Piedmont region, the effect is usually restricted to the immediate vicinity of the well, and as soon as the pump is shut off, the water level begins to return to its former level. The amount of drawdown varies considerably, depending on pumping rate, duration of pumping, and the hydrologic properties of the aquifer.

In some areas, rainwater infiltrating the ground encounters an impermeable barrier, saturating the material above the barrier. While the material below remains unsaturated. The surface of such a saturated zone is known as a perched water table. In the Piedmont, perched water tables are not as extensive as the main water table, and are usually temporary. They are not shown on this map.

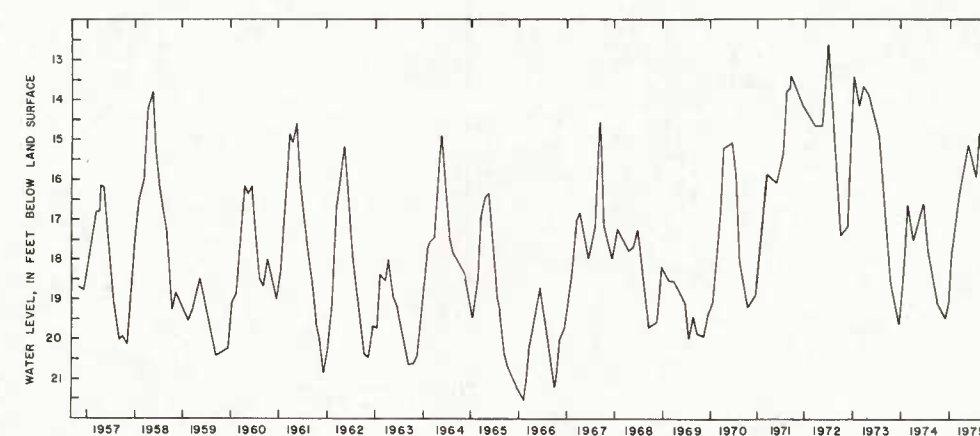
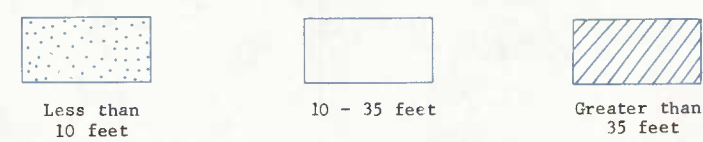
APPROXIMATE DEPTH TO WATER TABLE
BELOW LAND SURFACE

Figure 1.-- Hydrograph for well BA-CE 21.

SUPPLEMENTAL RECORD OF SPRINGS IN THE NEW FREEDOM QUADRANGLE

NUMBER	OWNER	ALTITUDE (in feet)	TOPOGRAPHIC SETTING	AQUIFER	YIELD	DATE	USE OF WATER
BA-AC 138	-	715	hillslope	300 Prettyboy Schist	5	04/06/1979	unused
BA-AC 139	-	730	hillslope	300 Prettyboy Schist	2	04/06/1979	unused
BA-AC 140	Md. State Parks	740	valley flat	300 Prettyboy Schist	5	03/21/1979	unused
BA-AC 141	-	740	hillslope	300 Prettyboy Schist	3	03/21/1979	unused
BA-AC 142	-	630	hillslope	300 Prettyboy Schist	3	03/21/1979	unused
BA-AC 143	-	750	hillslope	300 Prettyboy Schist	5	03/22/1979	unused
BA-AC 144	-	800	hillslope	300 Prettyboy Schist	4	03/24/1979	unused
BA-AC 145	-	760	upland draw	300 Prettyboy Schist	2	03/24/1979	unused
BA-AC 146	-	780	hillslope	300 Prettyboy Schist	2	03/24/1979	unused
BA-AC 147	-	690	hillslope	300 Prettyboy Schist	5	03/23/1979	unused
BA-AC 148	-	590	hillslope	300 Prettyboy Schist	2	03/24/1979	unused
BA-AC 149	-	690	hillslope	300 Prettyboy Schist	5	03/21/1979	unused
BA-AD 139	-	690	hillslope	300 Prettyboy Schist	2	03/26/1979	stock
BA-AD 140	-	700	hillslope	300 Prettyboy Schist	2	03/26/1979	unused
BA-AD 141	-	580	hillslope	300 Prettyboy Schist	1	03/26/1979	unused
BA-BC 262	-	680	hillslope	300 Prettyboy Schist	1	04/05/1979	unused
BA-BC 263	Baltimore City	560	hillslope	300 Prettyboy Schist	5	04/05/1979	unused
BA-BC 264	Baltimore City	570	hillslope	300 Prettyboy Schist	7	04/05/1979	unused
BA-BC 265	Baltimore City	560	hillslope	300 Prettyboy Schist	1	04/05/1979	unused
BA-BC 266	Baltimore City	560	hillslope	300 Prettyboy Schist	1	04/05/1979	unused
BA-BD 206	-	460	upland draw	300 Prettyboy Schist	2	03/20/1979	unused
BA-BD 207	-	520	hillslope	300 Prettyboy Schist	2	03/23/1979	unused
BA-BD 208	-	590	hillslope	300 Prettyboy Schist	3	03/23/1979	stock



AVAILABILITY OF GROUND WATER

by
Mark T. Duigon

NATURE OF OCCURRENCE

Ground water in the Piedmont province occurs chiefly in fractures in the crystalline metamorphic rocks, and in the pore spaces of the overlying, unconsolidated material. Intersecting fractures allow greater quantities of water to be removed. Fractures tend to become fewer in number and the voids formed by the fractures tend to become narrower with increased depth (LeGrand, 1954); consequently, the rate at which water can flow through the rocks, and the amount of water stored in the rocks decreases at greater depths. The optimum depth to drill a well also involves economic factors. Generally speaking, a domestic well in crystalline rock should be less than 250 ft deep (Davis and Turk, 1964). If a sufficient quantity of water is not obtained after drilling to this depth, the lower cost of drilling deeper rather than drilling elsewhere is offset by the lower probability of obtaining more water.

The water pumped from a well is commonly derived from storage in the overlying material (overburden) and transmitted through the rock fractures. The rocks themselves have little storage ability. The permeability and storage capacity, due to the network of fractures, controls the yield of a well.

The overburden provides renovation for downward-percolating water. Rock fractures have very little ability to renovate water. If contaminated water passes through an insufficient thickness of overburden, it can pass unpurified through the rock fractures and into a water-supply system.

Because a successful well must intersect water-bearing fractures, the selection of a well site should maximize the probability of drilling through fractures. Some rocks tend to fracture more readily than others; some rocks weather more readily, thereby enlarging existing fractures. The rocks underlying the New Freedom quadrangle area are relatively uniform schists (Prettyboy Schist, Pleasant Grove Schist, and Piney Run Formation; Crowley, 1976), so factors other than rock type affect well yield. Topography, in some cases, is related to major fracture zones, and can be readily assessed on a topographic map or in the field. Wells in valleys and draws generally have higher yields than wells on hilltops.

An analysis of linear features aids in selecting the optimum site for a well. In some places, these features, called lineaments, are related to zones of more intense fracturing. The features are identified by linear segments of stream channels, linear soil or vegetational tonal patterns, and alignment of some geologic features. They can be seen on topographic maps and aerial photographs, but need to be field-checked for verification. Although fractures can occur anywhere, the probability of drilling a well that will intersect at least one water-bearing fracture is increased by choosing a site suspected of being in a zone of greater fracture density.

EXPLANATION

All of the New Freedom quadrangle is equivalent to what has been mapped as Geohydrologic Unit 3 in adjacent quadrangles. Although it is considered one unit, there is a good deal of variability in yield. Only wells pumped for 3 or more hours were used to derive the tabulated statistics. This time period was selected because specific capacity (discharge, in gal/min, divided by drawdown, in ft) decreases with duration of pumping, but at a rate that also decreases with time.

3

GEOHYDROLOGIC UNIT 3: This is the most widespread unit in Baltimore County and comprises the entire New Freedom quadrangle, where it is composed predominately of the Prettyboy Schist, with a small area of Pleasant Grove Schist and Piney Run Formation in the southeast corner. The following table summarizes the basic well statistics for the New Freedom quadrangle.

	Range	Median	Mean	Standard deviation
Reported yield (gal/min)	0-22	4	5.7	5.25
Specific capacity (gal/min)/ft drawdown	0.00-3.5	.10	.34	.528
Well depth (ft)	57-525	160	183	90.62

NUMBER OF WELLS: 121

Figure 1 shows distribution of well yields calculated from specific capacities. Figure 2 is a cumulative frequency curve for specific capacity of wells in the New Freedom quadrangle.



Lineaments

- Well with reported yield less than 2 gal/min.
- Well with reported yield greater than 15 gal/min.

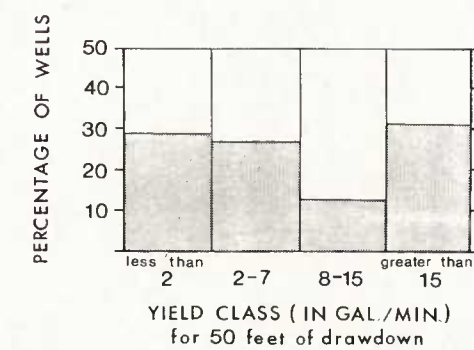


Figure 1.-- Distribution of well yields in the New Freedom quadrangle (121 wells).

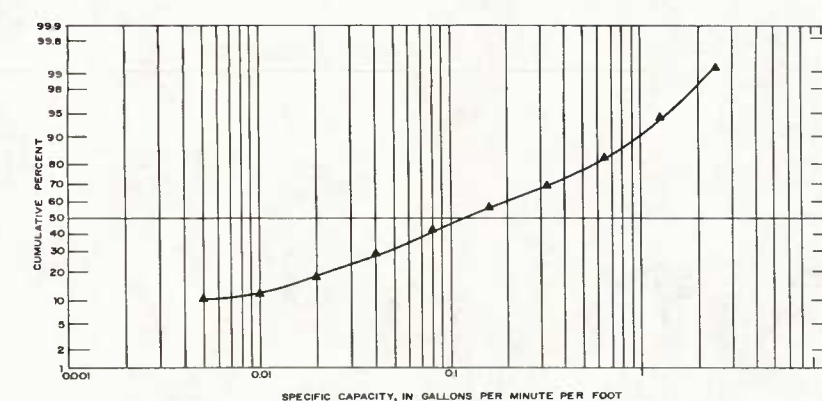
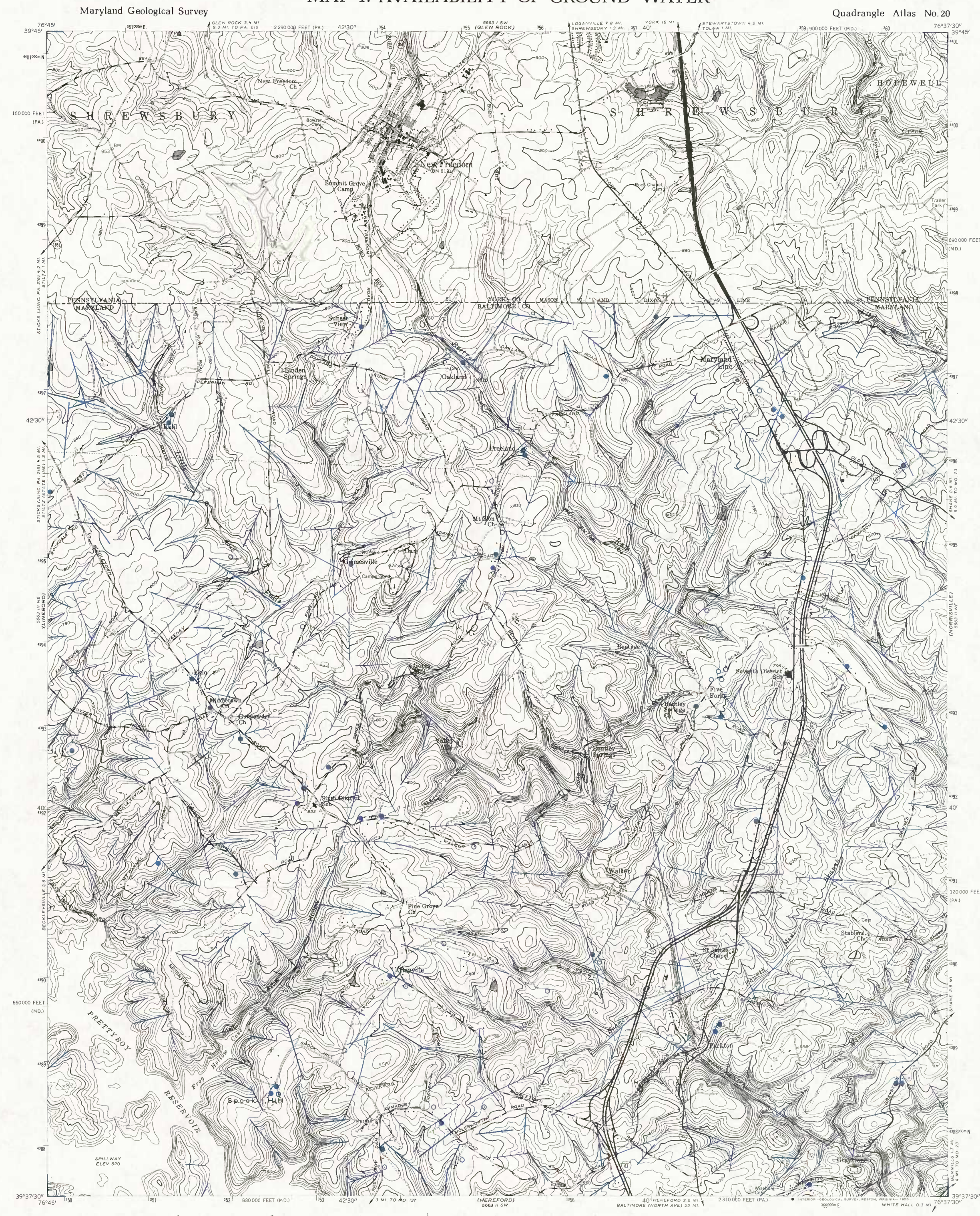


Figure 2.-- Cumulative distribution of well specific capacities in the New Freedom quadrangle (121 wells).

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MAP 4. AVAILABILITY OF GROUND WATER



Topography from aerial photographs by photogrammetric methods 1944. Aerial photographs taken 1945. Culture revised by the Geological Survey 1958. Photorevised 1974.

UTM GRID AND 1974 MAGNETIC NORTH DECLINATION AT CENTER OF SHEET

CONTOUR INTERVAL 20 FEET
NATIONAL GEODETIC VERTICAL DATUM OF 1929

1983



MAP 5. GEOHYDROLOGIC CONSTRAINTS ON SEPTIC SYSTEMS

Quadrangle Atlas No. 20

GEOHYDROLOGIC CONSTRAINTS
ON SEPTIC SYSTEMSBy
Mark T. Duigon

INTRODUCTION

Where centralized sewage systems are not available, wastes from individual homes must be disposed of in comparatively small areas within a lot. These wastes are composed of many different substances including urine, fecal matter, laundry detergents and cleaning compounds, and food scraps—all transported out of the house as a slurry by mixing with large quantities of water. These substances must be reduced in quantity or deactivated; otherwise, harmful conditions may become established in the environment, particularly in the water-supply system.

The usual disposal method is to pipe the slurry into a septic tank where the liquid is separated from solids and greases, and partial decomposition of some of the waste material occurs. The effluent is then directed into a seepage pit or tile field for distribution into soil. As the effluent percolates downward toward the water table, the soil filters and absorbs most deleterious substances.

Careful construction and maintenance of disposal systems are essential. Although it is recognized that these systems have a limited life span, failure is often accelerated by negligent construction and lack of periodic maintenance. Systems operating according to principles different from those described above may be more effective, but if not maintained properly, they may lose their effectiveness and fail more readily than conventional systems. (See, for example, Marshall, 1979, p. 24-25).

CONSTRAINT FACTORS

- Flood hazard:** Disposal systems do not drain properly when flooded and may be physically damaged. Contamination of surface water is possible when flood waters mix with effluent, and can spread to ground-water supplies.
- Shallow water table:** If effluent enters the ground-water system before it has passed through enough soil for adequate renovation, it will contaminate the system. Baltimore County requires a separation of 4 ft from the base of the seepage system to the water table.
- Depth to bedrock:** Fractures in bedrock act as ground-water conduits, and renovation of effluent is not effective. Therefore, a sufficient thickness of unconsolidated material between the base of the seepage system and the bedrock surface is required.
- Slope:** Steep slopes generally have a thin soil cover and are likely to allow effluent to emerge at the surface. Baltimore and Carroll Counties allow a maximum slope of 25 percent. Stuenkel (written commun., 1974) concluded that, where the slope exceeds 20 percent, effluent will come to the surface downslope from a drainfield regardless of soil type or depth of trenches. Slope categories for this map were obtained from Map 1.
- Infiltration rate:** This factor affects the design of the disposal system. If infiltration is too slow, drainage will be sluggish and effluent may back up through the plumbing system, or may appear at the surface due to flooding. If infiltration is too fast, renovation will be inadequate. In Maryland, the infiltration rate is evaluated at the site by a percolation test.

Most of these factors are individually evaluated on a broad scale by the U.S. Department of Agriculture, Soil Conservation Service (Reynold and Matthews, 1976). These evaluations are tabulated, providing the values of certain soil properties for each soil mapping unit. The map presented here integrates those evaluations in addition to field observations by the author, other data in this atlas, and consideration of percolation tests by county officials. This map cannot substitute for onsite evaluations, as discussed in the section, Limitations of Maps.

The percolation test in Baltimore County consists of digging at least two holes to bedrock or as deep as the backhoe will dig (about 15 ft). This is to determine if the water table or bedrock surface is high. A lateral extension of the first hole is dug to an approximate depth of 5 ft (initially), and, at the bottom, a lateral hole is hand-dug. This small hole is filled with water to a level of 7 in. above the base of the hole. The level is allowed to drop 1 in. and then is timed as it drops a second inch. The test is considered successful if the level takes from 7 to 30 minutes to drop the second inch. If the test fails, it is repeated at a greater depth or at another location. A proposed building lot must have a successful percolation test before a building permit will be issued, if sewage is to be disposed onsite. The testing health official also notes any other factors that may affect operation of the disposal system, such as impermeable layers.

MAP UNITS

UNIT I: Disposal facilities constructed in this unit face a high probability of failure. This unit generally occurs adjacent to streams and lakes, where the water table can be shallow and flooding can be a hazard. Other constraining factors are land slopes exceeding 25 percent and the presence of soils having low permeability (less than 0.63 in./hr, equivalent to greater than 95 min/in.). This unit includes soils developed on alluvium and subject to flooding, such as the Codorus silt loam and Harboro silt loam. It also includes steep Manor soils and thin, stony Mt. Airy soils.

UNIT II: Conditions in this unit are not as severe as in Unit I, but they may work in combination to adversely affect disposal systems. Because of its variability and marginality, onsite evaluation is of particular importance. Major soils in this unit are Manor and Glenelg soils having moderate (15 to 25 percent) slopes. Also included are variable areas of scattered outcrops and stony soils, and land which has been modified and, hence, is highly variable. Depths to water table and bedrock vary; for example, depth to bedrock beneath Manor soils is reported to be from 3 1/2 to 10 ft.

UNIT III: Conditions in this unit are generally most favorable for installation of disposal systems. Onsite inspection is still required for characteristics of particular sites. The unit generally covers well-drained interfluvial areas dominated by Chester, Manor, and Glenelg soils having slopes less than 15 percent. Permeability varies (0.63 to 6.3 in./hr or 95 to 9.5 min/in.), but is generally adequate. The water table and bedrock are generally at depths greater than 10 ft from land surface.

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Topography from aerial photographs by photogrammetric methods 1944. Aerial photographs taken 1943. Culture revised by the Geological Survey 1958. Photorevised 1974.

HYDROGEOLOGIC ATLAS NO. 20
NEW FREEDOM QUADRANGLE, MARYLAND

By
Mark T. Duigon

INTRODUCTION

This atlas describes the hydrogeology of the New Freedom 7 1/2-minute quadrangle in northern Baltimore County, Maryland (fig. 1). The information contained herein is intended for use by planners, health officials, developers, environmental consultants, and anyone else concerned with baseline hydrogeologic data and the effects of hydrogeologic factors on development.

The climate of this area is humid temperate, with an average annual temperature of 52°F and an average annual precipitation of 44 in. (Vokes and Edwards, 1974, p. 20, 28).

The New Freedom quadrangle lies within the eastern division of the Piedmont physiographic province. The land surface is generally undulating, but some sections of stream valleys are deeply dissected. The drainage pattern shows some control by joints and fractures in the bedrock.

The entire Maryland portion of the area is drained by tributaries of Gunpowder Falls. A portion of Prettyboy Reservoir, formed by a dam on the Gunpowder Falls, is in the southwest corner of the area.

The northern portion, in Pennsylvania, drains into the Susquehanna River via several tributaries. These rivers ultimately empty into Chesapeake Bay.

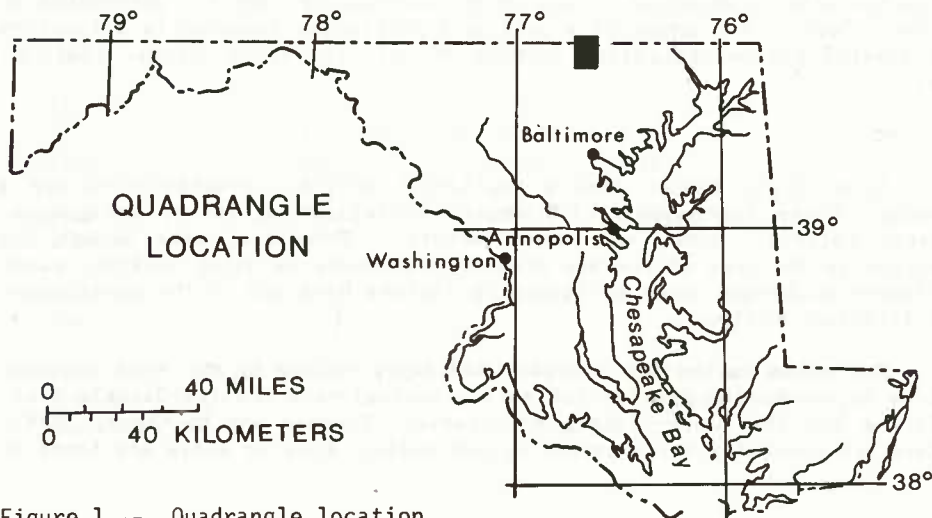


Figure 1.-- Quadrangle location

A permanent gaging station, located approximately 1 1/2 mi southeast of Graystone, monitors discharge from Little Falls, the major tributary in the New Freedom quadrangle area. Low-flow measurements have been conducted on Beetree Run at Bentley Springs.

Interstate 83 (Harrisburg, Pa., to Baltimore, Md.) runs north-south through the quadrangle area. It runs parallel to York Road (Md. Rte. 45), but allows much more rapid transportation. For this reason, residential development serving the needs of commuters working in the Baltimore area has been rapidly increasing in northern Baltimore County. Farming remains important; corn is the chief crop, and dairy products are also important.

GEOLOGY and SOILS

The stratigraphic nomenclature used in this report is that proposed by Crowley (1976) and does not necessarily follow the usage of the U.S. Geological Survey. The chief difference between this terminology and previous usage (Higgins, 1972) is the manner in which the Wissahickon Formation has been subdivided.

Prettyboy Schist underlies most of the mapped area, except for a band of Pleasant Grove Schist and a wedge of the garnet facies of the Loch Raven Schist in the southeast corner. These rocks are of early Paleozoic age. Fine-grained sediments derived from the southeast accumulated in a down-warping basin, and were deformed and faulted by powerful forces that moved large areas, or plates, of crustal rock. This activity, known as plate tectonics, generated enormous quantities of heat and pressure, resulting in a seemingly jumbled assortment of metamorphic rocks.

Later earth movements uplifted these rocks, exposing them to the mechanisms of weathering and erosion. These processes began in Mesozoic time and continue to this day; in fact, the development of agriculture has accelerated erosion in some areas.

The altered material formed at the surface of rock (or sediments) is known as soil. The nature of a soil at a particular location is a function of several parameters called factors of soil formation (Jenny, 1941, p. 16):

$$s = f (cl, o, r, p, t, \dots)$$

This simply states that a particular soil's characteristics are a result of the interaction of climate, biological activity, topography, parent material, time, and other factors. Therefore, even though the bedrock in the area of the New Freedom quadrangle is quite uniform, minor differences in the other soil-forming factors have led to the development of different soils.

The soils in the New Freedom quadrangle belong to two soil associations (areas having distinctive soil patterns)--the Chester-Glenelg Association and the Manor-Glenelg Association (Reybold and Matthews, 1976). These are generally well-drained upland soils. Chester soils are found on

hilltops and ridgetops. Manor and Glenelg soils more frequently have steeper slopes than Chester soils, and where adjacent to Chester soils, are found downslope. Minor soils, such as Baile, Glenville, Codorus, and Hatboro, are found in upland draws and flood plains. Other minor soils, found on ridgetops or upper slopes, include the Elioak and Mt. Airy series. Differences in these soils affect the success and suitability of certain land uses.

HYDROLOGY

Ground water, stored in the intergranular pore spaces of unconsolidated soil material (overburden), is transmitted through the crystalline rocks of the Piedmont by means of fractures. Most wells in the Piedmont are drilled through the overburden and into fresh rock. The amount of water produced by such a well depends, in part, on the number of fractures that the hole intersects, and the extent of the network of intersecting fractures. Figure 2 is a generalized Piedmont setting showing the hydro-geologic factors involved in well performance.

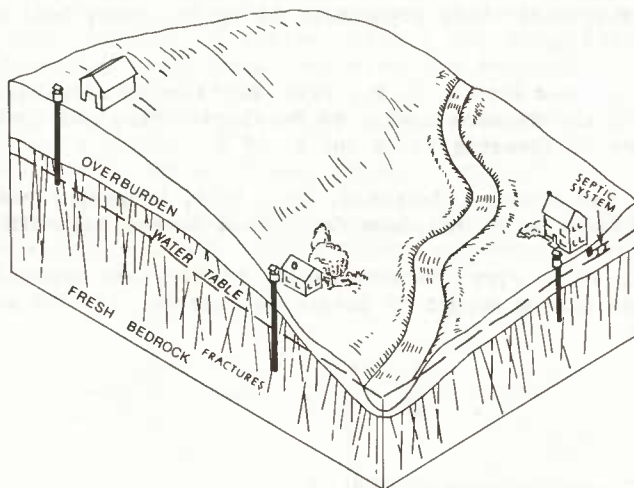


Figure 2.-- Wells in the Maryland Piedmont.

The generalized pattern of water circulation is known as the hydro-logic cycle (fig. 3). The hydrologic cycle is the combination of "paths" that a quantity of water may move along as it is recycled through the earth and atmosphere. Water may be temporarily detained, but net losses or gains to the hydrologic cycle are negligible. A quantitative evaluation of the

hydrologic cycle in a particular region can be made by use of the hydrologic budget:

$$P = R + ET + \Delta S$$

where

P = precipitation,

R = runoff,

ET = combined evaporation and transpiration, and

ΔS = change in storage.

Precipitation is the source of water in the Piedmont and is balanced by losses due to surface flow (runoff), release back into the atmosphere as water vapor (evapotranspiration), and changes (gain or loss) in the amount of water in storage in the ground.

Water quality is affected by the substances with which the water comes into contact. Ground water usually dissolves some of the minerals present in the rock and soil through which it passes. The intended use determines the suitability of water of a particular chemical nature: Water that is fit to drink may not be suitable for certain industrial applications such as steam boilers.

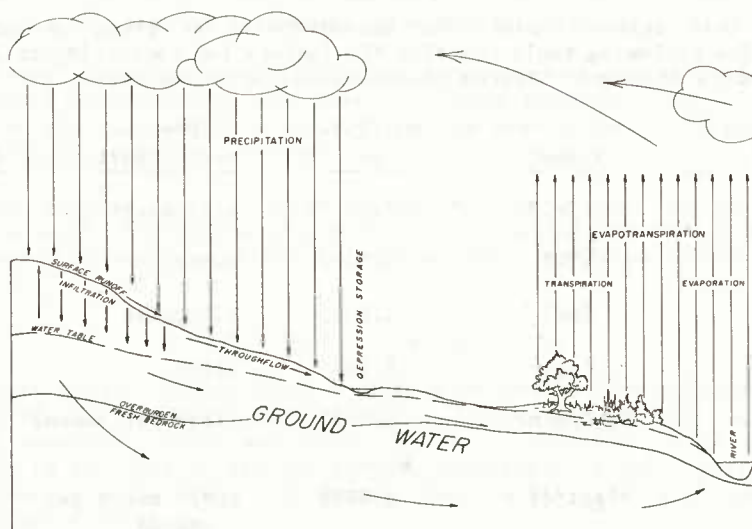


Figure 3.-- The hydrologic cycle.

MAPS INCLUDED IN THIS ATLAS

The information in this atlas is presented as five maps, each prepared on a standard 7 1/2-minute topographic quadrangle base.

1. Slope of the Land Surface, by Maryland Geological Survey.
2. Location of Wells and Springs, by Mark T. Duigon.
3. Depth to the Water Table, by Mark T. Duigon.
4. Availability of Ground Water, by Mark T. Duigon.
5. Geohydrologic Constraints on Septic Systems, by Mark T. Duigon.

LIMITATIONS OF MAPS

These maps are designed for broad planning purposes and are not intended to substitute for detailed onsite investigations where required. Boundaries may not be exact because of map scale, data quality, geographical distribution, and judgment required for interpolation.

CONVERSION OF MEASUREMENT UNITS

In this atlas, figures for measurements are given in inch-pound units. The following table contains the factors for converting these inch-pound units to metric (System International or SI) units:

<u>Inch-pound Unit</u>	<u>Symbol</u>	<u>Multiply by</u>	<u>For Metric Unit</u>	<u>Symbol</u>
inch	(in.)	25.40	millimeter	(mm)
foot	(ft)	0.3048	meter	(m)
mile	(mi)	1.609	kilometer	(km)
gallon	(gal)	3.785	liter	(L)
gallon per minute	(gal/min)	0.0631	liter per second	(L/s)
gallon per day	(gal/d)	0.0438	cubic meter per second	(m ³ /s)
gallon per minute per foot	[(gal/min)/ft]	0.2070	liter per second [(L/s)/m] per meter	

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^{1/} The name of this agency was changed to the Maryland Geological Survey in June 1964.